Globally Optimal Nonlinear Model Predictive Control

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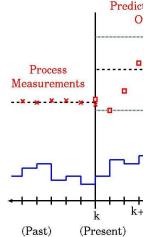
Presentation Outline

- Background and Motivation
- Nonlinear Model Predictive Control
 - > Formulation
 - ➤ Deterministic Method for Solving Nonconvex Problem
- Case Study
 - ➤ Isothermal CSTR with Van de Vusse kinetics
- Summary

Model Predictive Control (MPC)

(Garcia, Prett, and Morari, 1989)

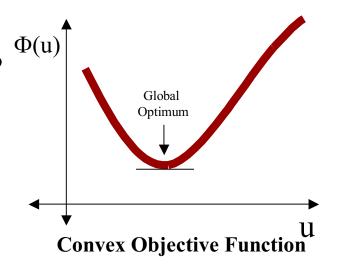
- Model Predictive Control is an advanced control algorithm that handles:
 - Multivariable interacting systems
 - Soft constraints on both inputs and outputs
 - Measured disturbances
 - Process time delays and difficult dynamics
 - Known future setpoint changes (reference transitions)
- Limitations
 - Requires an explicit model of the process
 - Need to solve a constrained optimization problem online
- 1. Using process data, formulates an optimization problem.
- 2. Solves the problem online and implements the optimal control move.
- 3. Waits for new data at next time step.



Linear vs. Nonlinear Formulations

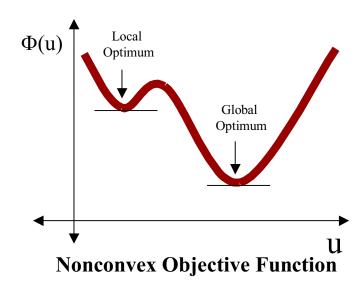
Linear Formulations:

- Mismatch between linear model and nonlinear process can lead to poor closed-loop performance and/or instability.
- Linear model (linear constraints) convex problem (only one minimum)
- Efficient solvers (local) exist to solve the convex problem



Nonlinear Formulations:

- Nonlinear model handles process nonlinearities.
- Nonlinear model (nonlinear constraints)
 nonconvex problem (multiple minima)
- Local solvers left susceptible to choosing suboptimal minima.
- Need to guarantee global optimality in nonconvex problems.



Nonlinear Model Predictive Control (NMPC) Formulation



$$\Phi = \sum_{i=1}^{p} \Gamma_{e} e(i) + \sum_{i=1}^{m} \Gamma_{u} \Delta u(i)$$

Constrained Optimization Problem:

$$\min_{\{u(i),\dots u(m)\}} \mathbf{\Phi}$$

subject to:

$$x(k+1) = f(x(k), u(k))$$

$$y(k) = g(x(k), u(k))$$

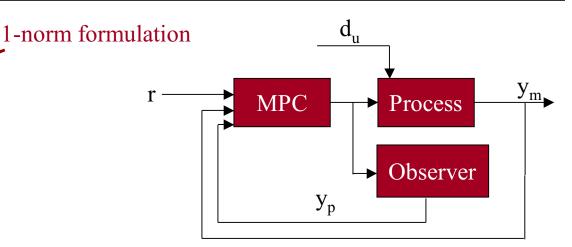
Nonlinear Process Model

$$|r(i) - y(i)| \le e(i)$$
 $\forall i = 1 \dots p$ Error Terms

 $|u(i-2)-u(i-1)| \le \Delta u(i-1) \quad \forall i=1...m \quad \Delta u \text{ terms}$

$$d(i) = y_m(0) - y_p(0)$$
 Disturbance Update

$$u^L \le u \le u^U$$
 Actuator Limits

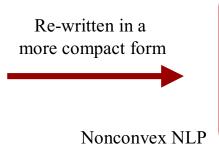


r = reference (setpoint)

 y_m = measured output

 d_{ij} = unmeasured disturbance

 y_p = predicted output



$$\min_{x} C^{T} x$$

$$s.t. Ac \leq l$$

$$f(x) = 0$$

$$x^L \le x \le x^U$$

Online vs. Offline Methods for MPC

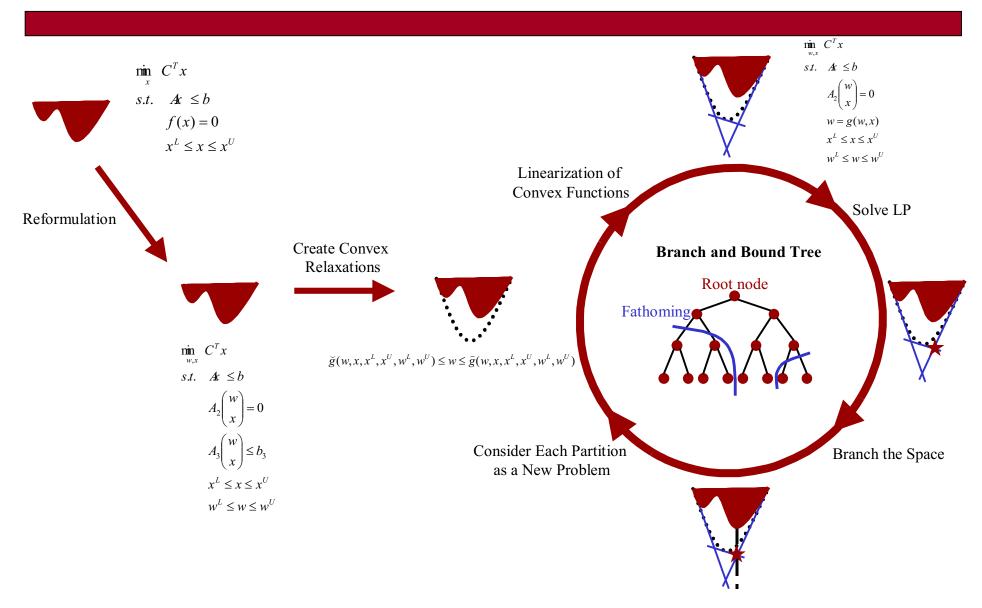
Online

- Formulate the appropriate optimization problem based on current data at each time step.
- Solve the problem online.
 - computationally demanding
 - real-time constraints
- Possibility of unnecessarily solving the same problem over and over again
- Solution is optimal and pertains exactly to the process' current state.

Offline

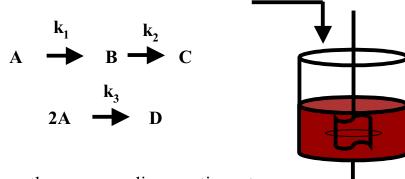
- Partition solution space into characteristic regions based on a set of parameters (states, inputs, etc...)
- Solve problems from each region offline
 - high dimensionality issues
 - Can you foresee all scenarios?
- At each time step, identify appropriate region online based on current data and "look up" the solution.
 - low online computational demand
- Implement solution from the region.
 - Suboptimal?

Deterministic Method for Solving the Nonconvex NLP



Benchmark Control Problem

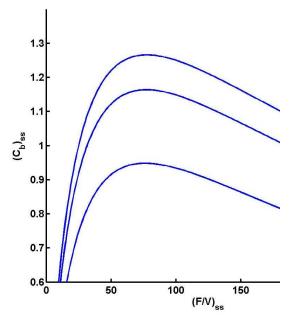
Consider the isothermal operation of a SISO two state CSTR exhibiting Van de Vusse kinetics:



Where the corresponding reaction rates are:

$$r_A = -k_1 C_A - k_3 C_A^2$$

 $r_R = k_1 C_A - k_2 C_R$



Steady State Loci for the Reactor Operation at Different Feed Concentrations (C_{AO}) Exhibiting the Presence of an Input Multiplicity

The system can be described by:

$$\frac{dC_A}{d} = \left(\frac{F}{V}\right) (C_{AO} - C_A) - k_1 C_A - k_3 C_A^2$$

$$\frac{dC_B}{d} = k_1 C_A - k_2 C_B - \left(\frac{F}{V}\right) C_B$$

where:

here:

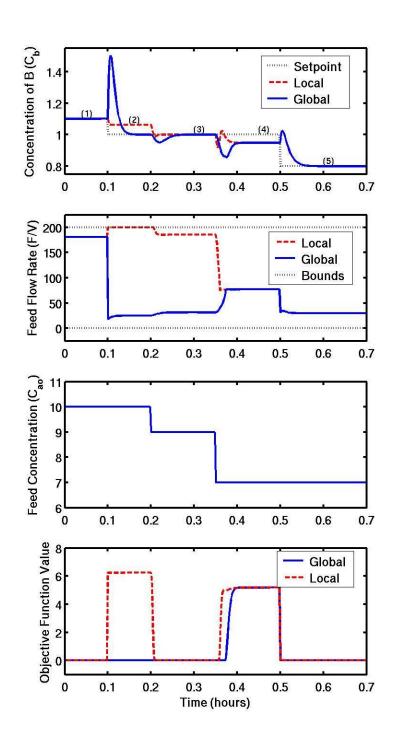
$$C_A = Conc. \text{ of Species A} = process \text{ state } (x_1)$$
 $C_B = Conc. \text{ of Species B} = process \text{ output } (y=x_2)$
 $k_i = Reaction Rate Constants$
 $F = Feed Flow Rate$
 $V = Reactor Volume (constant)$
 $C_{AO} = Conc. \text{ of A in the Feed}$
 $(F/V) = process \text{ input } (u)$

Closed-loop Performance Test

Both setpoint tracking and disturbance rejection are tested through a series of setpoint transitions and disturbance loads.

Assume the process is initially being operating where:

```
process input (u)
Feed Flow Rate/Reactor Volume (F/V)
                                                  = 181 mol/liter-hr
                                                                             process output (y)
Conc. of B (C_B)
                                                  = 1.1 \text{ mol/liter}
                                                                             disturbance (d)
Conc. of A in the Feed (C_{AO})
                                                  = 10 \text{ mol/liter}
y_{sp} = 1.1
                       y_{sp} = 1.0
C_{AO}=10
                                                                          y_{sp} = 0.8
                                   C_{AO} = 9
                                                        C_{AO} = 7
                                                                                               hrs
               t = 0.1
                             t=0.2
                                                       t = 0.4
                                                                    t=0.5
   t=0
                                          t=0.3
                                                                                  t=0.6
```



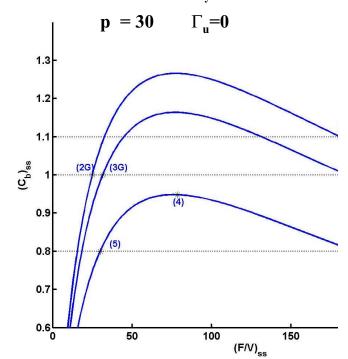
Closed-loop Results

(single degree of freedom)

Objective Function:

$$\Phi = \Gamma_{y} e(p) + \sum_{i=1}^{m} \Gamma_{u} \Delta u(i)$$
terminal weight

Tunings: m = 1 $\Gamma_v = 100$



Steady State Loci for the Reactor Operation at Different Feed Concentrations (C_{AO}) Exhibiting the Presence of an Input Multiplicity

Sample Optimization Problem

Assume the process is operating at:

u = 181 mol/liter-hr y = 1.1 mol/liter $C_{AO} = 10 \text{ mol/liter}$

Consider the Objective Function as

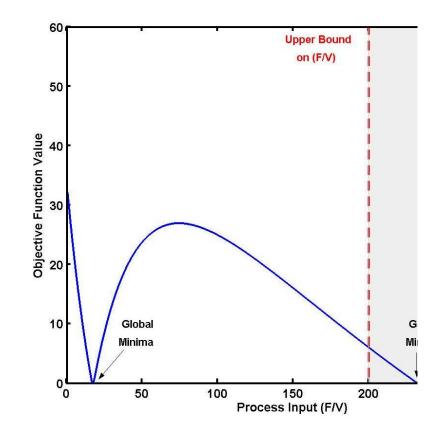
$$\Phi = \Gamma_{y} e(p) + \sum_{i=1}^{m} \Gamma_{u} \Delta u(i)$$

(terminal weight)

Let: m = 1 $\Gamma_y = 100$ p = 30 $\Gamma_u = 0$

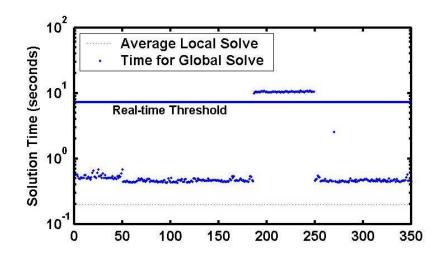
Assume bounds on the input.

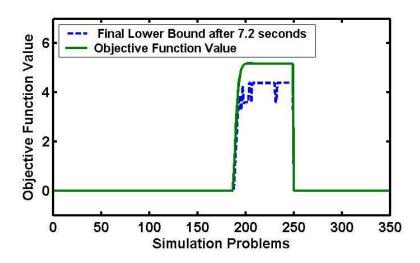
 $0 \le u \le 200$



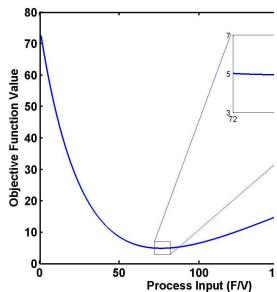
Sample objective function for problem having the setpoint moved from the initial condition of 1.1 mol/liter to 1 mol/liter.

Real-Time Considerations





- \triangleright Sampling Time = 7.2 seconds
- ➤ Must terminate solves to meet realtime constraints.
- ➤ Global solution might have been found, not guaranteed.



Sample objective function for a problem that takes longer than 7.2 seconds to solve globally.

Concentration of B (C_b) Setpoint Local Global DUCKNOOUTO 0.1 0.3 0.4 0.5 0.6 200 Feed Flow Rate (F/V) --- Local Global Junaari 0.2 0.3 0.5 0.6 0.7 Feed Concentration (C_{ao}) 0.1 0.2 0.3 0.4 0.5 0.6 0.7 Objective Function Value Global --- Local 0.1 0.2 0.3 0.4 0.5 0.6 0.7 Time (hours)

Closed-loop Results

(multiple degrees of freedom)

Objective Function:

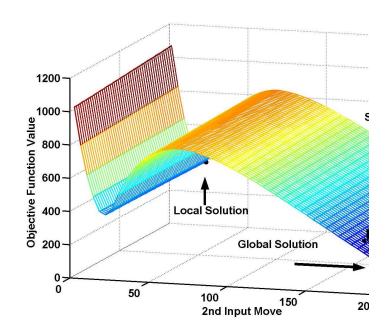
$$\Phi = \sum_{i=1}^{p} \Gamma_{y} e(i) + \sum_{i=1}^{m} \Gamma_{u} \Delta u(i)$$

Tunings: m = 2

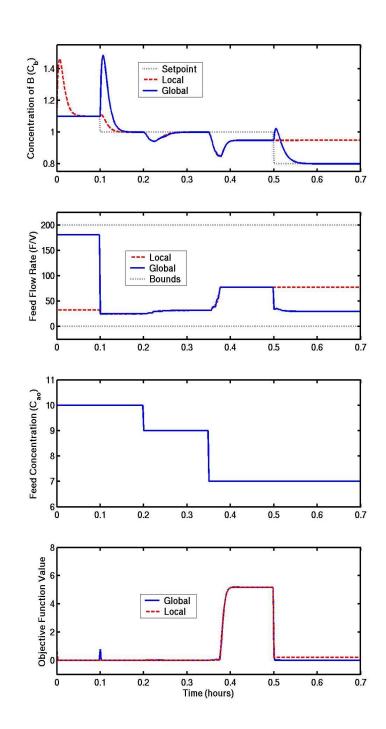
$$\Gamma_{\rm y} = 100$$

$$p = 30$$

$$\Gamma_{\rm u} = 0.005$$



Sample objective function at the time of the first setpoint change for the NMPC with two degrees of freedom (m=2)



Use of a Terminal Weight

(multiple degrees of freedom)

Objective Function:

Tunings:

$$\Phi = \Gamma_{y}e(p) + \sum_{i=1}^{m} \Gamma_{u}\Delta u(i)$$

$$\mathbf{m} = \mathbf{2} \qquad \Gamma_{y}=\mathbf{100}$$

$$\mathbf{p} = \mathbf{30} \qquad \Gamma_{u}=\mathbf{0.005}$$
terminal weight

As in the single degree of freedom (m=1) case, the modified objective function (using the terminal weight) allows for the controller to better track the setpoint.

Concentration of B (C_b) Setpoint --- Local - Global 200 Feed Flow Rate (F/V) --- Local Global **Bounds** 0.2 0.6 0.1 0.3 0.4 0.5 0.7 Feed Concentration (C_{ao}) 0.1 0.2 0.3 0.4 0.5 0.6 0.7 Objective Function Value Global 0.7 0.1 0.2 0.3 0.4 0.5 0.6 Time (hours)

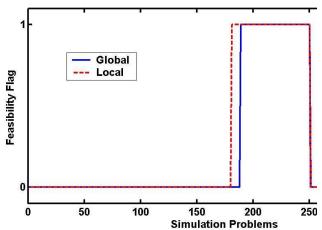
Incorporating Hard Constraints

Objective Function:

$$\Phi = \Gamma_{y} e(p) + \sum_{i=1}^{m} \Gamma_{u} \Delta u(i)$$

Tunings:
$$m = 2$$
 $\Gamma_y = 100$ $e(p) = 0$ $\rho = 30$ $\Gamma_u = 0.005$

Possibility for Infeasible Problems (constraint relaxation may be necessary!)



Problem feasibility when a hard constraint is imposed on e(p). A value of 0 indicates feasible problems, while a value of 1 shows infeasible problems in which a hard constraint relaxation is necessary.

Setpoint Concentration of B (C_b) --- Local Global MANAGE ! 0.7 200 Feed Flow Rate (F/V) -- Local Global Bounds LANGERICA 0.2 0.3 0.4 0.5 0.6 Feed Concentration (C_{ao}) 0.2 0.3 0.4 0.5 0.6 0.7 0.1 500 Objective Function Value Global --- Local 0.2 0.4 0.6 Time (hours)

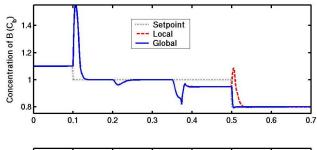
Traditional Objective Function with Hard Constraint

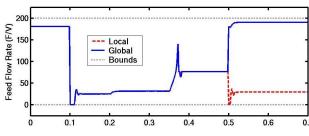
Objective Function:
$$\Phi = \sum_{i=1}^{p} \Gamma_{y} e(i) + \sum_{i=1}^{m} \Gamma_{u} \Delta u(i)$$

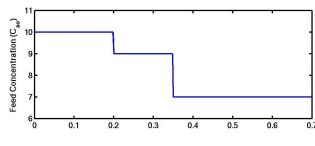
Tunings:
$$m = 2$$
 $\Gamma_y = 100$
 $p = 30$ $\Gamma_u = 0.005$ $e(p) = 0$

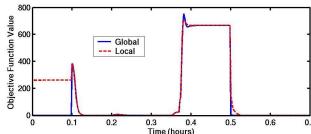
Improvement over using the traditional objective function without the hard constraint.

Noise Run









Objective Function

$$\Phi = \sum_{i=1}^{p-1} \Gamma_{y} e(i) + \Gamma_{T} e(p) + \sum_{i=1}^{m} \Gamma_{u} \Delta u(i)$$



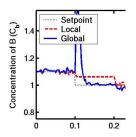
e(p) weighted more heavily than other errors.

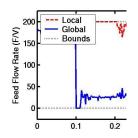
Tunings

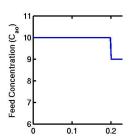
$$m = 2$$
 $\Gamma_y = 100$

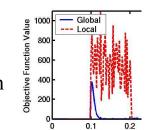
$$p = 30$$
 $\Gamma_u = 0.005$

$$\Gamma_{\rm T} = 10,000$$









Noise

➤ white measurement noise with a standard deviation of 3%

Summary

- ➤ A NMPC algorithm using a deterministic global optimization search method is proposed.
- ➤ The deterministic approach guarantees global optimums to the nonconvex NLPs associated with the NMPC formulation.
- The algorithm eliminates poor performance in the CSTR example resulting from suboptimal input trajectories provided by local solution techniques.
- The proper objective function and controller tunings must be utilized to achieve the desired closed-loop results.
- Considerations must be made for cases where the desired solution cannot be obtained sufficiently fast for real-time use.

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